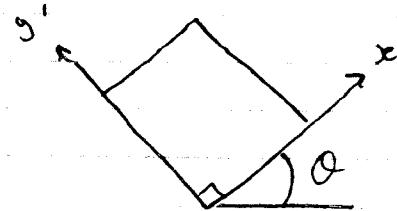


$\epsilon_x, \epsilon_y, \tau_{xy}$



$\epsilon_{x'}, \epsilon_{y'}, \tau_{x'y'}$

$$\left\{ \begin{array}{l} \epsilon_{x'} = \epsilon_{avg} + \frac{\epsilon_x - \epsilon_y}{2} \cos 2\theta + \frac{\tau_{xy}}{2} \sin 2\theta \\ \epsilon_{y'} = \epsilon_{avg} - \frac{\epsilon_x - \epsilon_y}{2} \cos 2\theta - \frac{\tau_{xy}}{2} \sin 2\theta \\ \frac{\tau_{x'y'}}{2} = \frac{\epsilon_x - \epsilon_y}{2} \sin 2\theta + \frac{\tau_{xy}}{2} \cos 2\theta \end{array} \right.$$

Principal strains:

$$\tan 2\theta_p = \frac{(\tau_{xy}/2)}{(\epsilon_x - \epsilon_y)/2} = \frac{\tau_{xy}}{\epsilon_x - \epsilon_y}$$

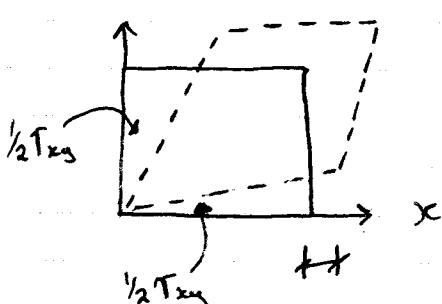
$$\epsilon_{1,2} = \epsilon_{avg} \pm R$$

$$\epsilon_{avg} = \frac{\epsilon_x + \epsilon_y}{2}, \quad R = \sqrt{\left(\frac{\epsilon_x - \epsilon_y}{2}\right)^2 + \left(\frac{\tau_{xy}}{2}\right)^2}$$

Max in-plane shear strain:

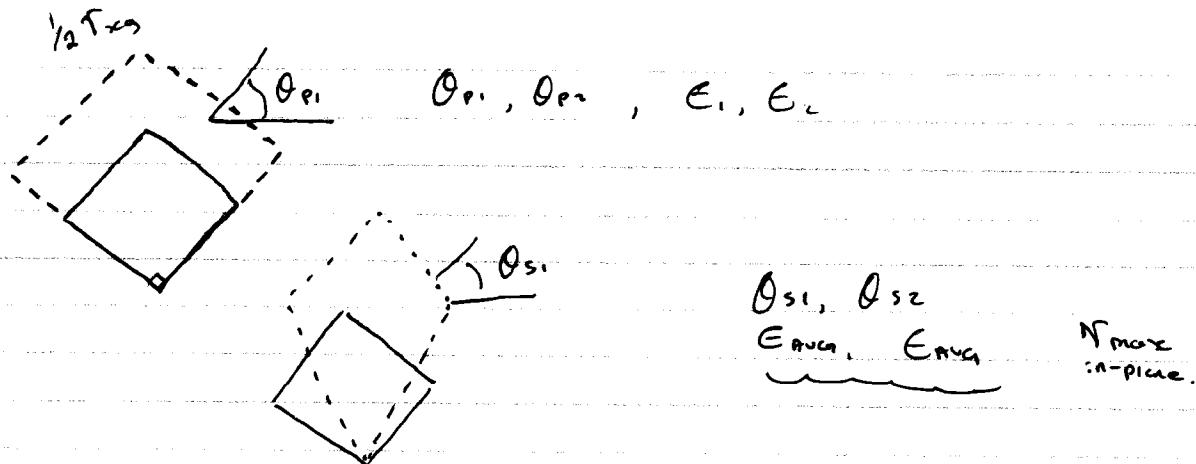
$$\frac{1}{2} \tau_{max \text{ in-plane}} = R = \sqrt{\left(\frac{\epsilon_x - \epsilon_y}{2}\right)^2 + \left(\frac{\tau_{xy}}{2}\right)^2}$$

$$\tan 2\theta_s = -\frac{\epsilon_x - \epsilon_y}{\tau_{xy}}$$

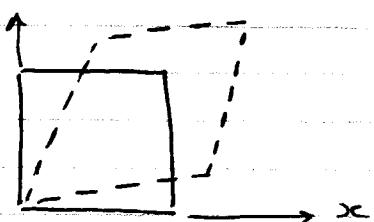


$\epsilon_x, \epsilon_y, \tau_{xy}$

(2)



Example



$$\begin{aligned} \epsilon_x &= 0 \\ \epsilon_y &= 0 \\ \tau_{xy} &= 200(10^{-6}) \end{aligned}$$

Find the state of strain on an element oriented at the point C.C.W. 45°

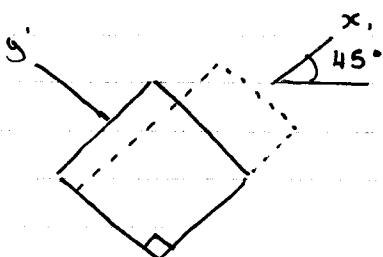
Solution: $\theta = 45^\circ$

$$\begin{aligned} \epsilon_x' &= \epsilon_{\text{AVG}} + \frac{\epsilon_x - \epsilon_y}{2} \cos 2\theta + \frac{\tau_{xy}}{2} \sin 2\theta \\ &= 0 + 0 + \frac{200(10^{-6}) \sin 90^\circ}{2} \end{aligned}$$

$$\epsilon_x' = 100(10^{-6}) (\tau)$$

$$\epsilon_y' = -100(10^{-6}) (c)$$

$$\begin{aligned} \gamma_2 \tau_{x'y'} &= -\frac{\epsilon_x - \epsilon_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta \\ &= 0 + 0 \Rightarrow 0 \end{aligned}$$



Example $E_x = -350 (10^{-6})$
 $E_y = 200 (10^{-6})$
 $T_{xy} = 80 (10^{-6})$

Determine:

- The principle strains and associated orientations
- The max in-plane shear strain and orientation

$$E_{avg} = -75 (10^{-6})$$

$$R = 277.9 (10^{-6})$$

$$\therefore E_1 = E_{avg} + R = (-75 + 277.9) (10^{-6}) \\ = 202.9 (10^{-6})$$

$$E_2 = E_{avg} - R \\ = -352.9 (10^{-6})$$

$$\tan 2\theta_p = \frac{T_{xy}}{E_x - E_y} = \frac{80 (10^{-6})}{(-350 - 200) (10^{-6})} \\ = -0.1445$$

$$2\theta_p = -8.28^\circ \text{ and } -8.28^\circ + 180^\circ$$

$$\theta_p = -4.14^\circ \text{ and } 85.86^\circ$$

When $\theta = -4.14^\circ$

$$E_{x'} = E_{avg} + \frac{E_x - E_y \cos 2\theta}{2} + \frac{T_{xy} \sin 2\theta}{2} \\ = \left[-75 + \frac{-350 - 200}{2} \cos(-8.28^\circ) + \frac{80}{2} \sin(-8.28^\circ) \right] \cdot 10^{-6} \\ = -352.9 (10^{-6}) = E_z \\ \therefore \theta_{p1} = 85.86^\circ \text{ and } \theta_{p2} = -4.14^\circ$$

- b) Max in-plane shear

$$\frac{1}{2} T_{max} = R = 277.9 (10^{-6})$$

$$T_{max} = 2R = 555.8 (10^{-6})$$

$$\tan 2\theta_s = -\frac{E_x - E_y}{T_{xy}} \\ = -\left(\frac{-350 - 200}{80}\right) \\ = 6.875$$

$$2\theta_s = 81.72^\circ \text{ and } 81.72^\circ + 180^\circ$$

$$\theta_s = 40.86^\circ \text{ and } 130.86^\circ$$

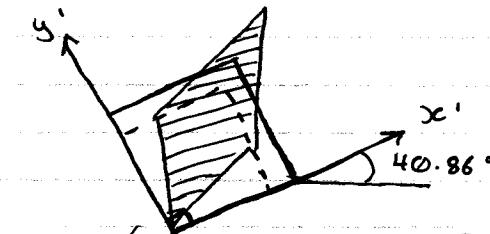
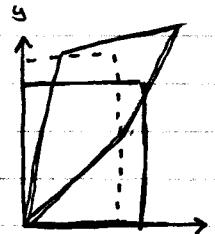
(4)

When $\theta = 40.86^\circ$

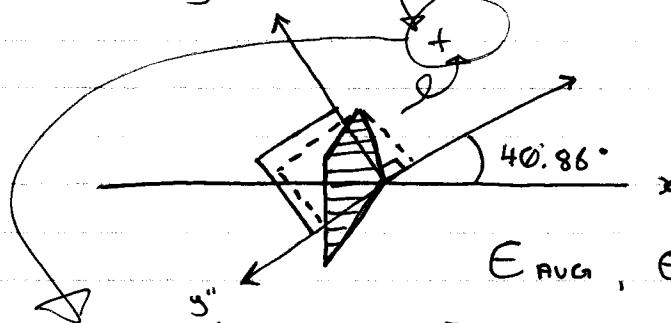
$$(2) \tau_{x'y'} = 277.9 (10^{-6})$$

$$\theta_{s1} = 40.86^\circ$$

$$\theta_{s2} = 130.86^\circ$$

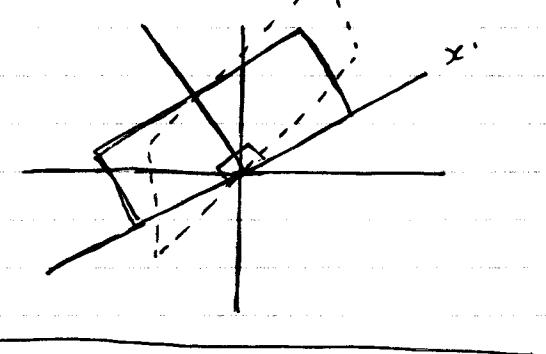


$$E_y, E_x, \tau_{xy}, x''$$

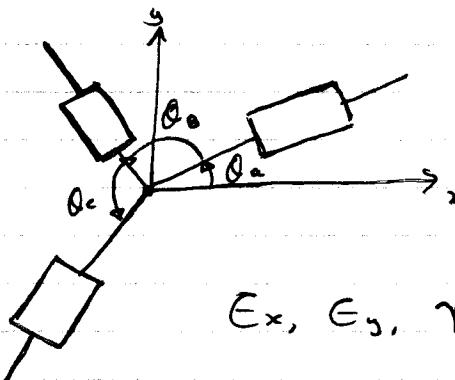


$$E_{avg}, E_{avg}, \tau_{x'y'}$$

$$E_{avg}, E_{avg}, \tau_{x'y'}$$



Strain Rosettes

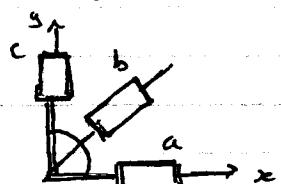


$$E_x, E_y, \tau_{xy}$$

Transformation

$$\left\{ \begin{array}{l} E_a = E_x \cos^2 \theta_a + E_y \sin^2 \theta_a + \tau_{xy} \sin \theta_a \cos \theta_a \\ E_b = E_x \cos^2 \theta_b + E_y \sin^2 \theta_b + \tau_{xy} \sin \theta_b \cos \theta_b \\ E_c = E_x \cos^2 \theta_c + E_y \sin^2 \theta_c + \tau_{xy} \sin \theta_c \cos \theta_c \end{array} \right.$$

Case 1:



$$\theta_a = 0^\circ$$

$$\theta_b = 45^\circ$$

$$\theta_c = 90^\circ$$

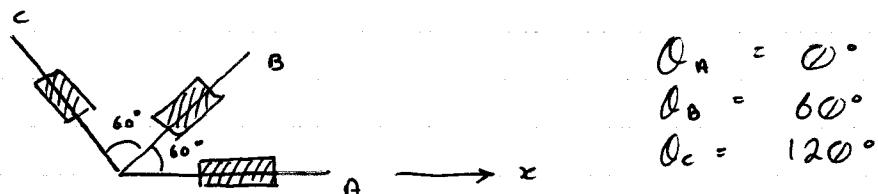
$$E_x = E_a \quad E_y = E_c$$

and

$$\begin{aligned} E_b &= E_x \cos^2 \theta_b + E_y \sin^2 \theta_b + T_{xy} \sin \theta_b \cos \theta_b \\ &= E_a \cos^2 45^\circ + E_c \sin^2 45^\circ + T_{xy} \sin 45^\circ \cos 45^\circ \\ &= \frac{1}{2} E_a + \frac{1}{2} E_c + \frac{1}{2} T_{xy} \end{aligned}$$

$$T_{xy} = 2E_b - E_a - E_c$$

Case 2 :



$$\theta_A = 0^\circ$$

$$\theta_B = 60^\circ$$

$$\theta_C = 120^\circ$$

$$\therefore E_x = E_a$$

$$\left\{ \begin{array}{l} E_b = E_x \cos^2 60^\circ + E_y \sin^2 60^\circ + T_{xy} \sin 60^\circ \cos 60^\circ \\ E_c = E_x \cos^2 120^\circ + E_y \sin^2 120^\circ + T_{xy} \sin 120^\circ \cos 120^\circ \end{array} \right.$$

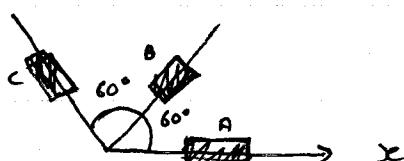
$$E_y = \frac{1}{3} (2E_b + 2E_c - E_a)$$

$$T_{xy} = \frac{2}{\sqrt{3}} (E_b - E_c)$$

Example :

$$\left. \begin{array}{l} E_a = 60 (10^{-6}) \\ E_b = 135 (10^{-6}) \\ E_c = 264 (10^{-6}) \end{array} \right\}$$

Determine principle strains and orientations.



From previous lecture -

Determine the principal strains and orientations.

Solution : $\begin{cases} \epsilon_x = \epsilon_a \\ \epsilon_y = \frac{1}{3}(2\epsilon_b + 2\epsilon_c - \epsilon_a) \\ \tau_{xy} = \frac{2}{\sqrt{3}}(\epsilon_b - \epsilon_c) \end{cases}$

$$\Rightarrow \epsilon_x = 60(10^{-6})$$

$$\epsilon_y = 246(10^{-6})$$

$$\tau_{xy} = -149(10^{-6})$$

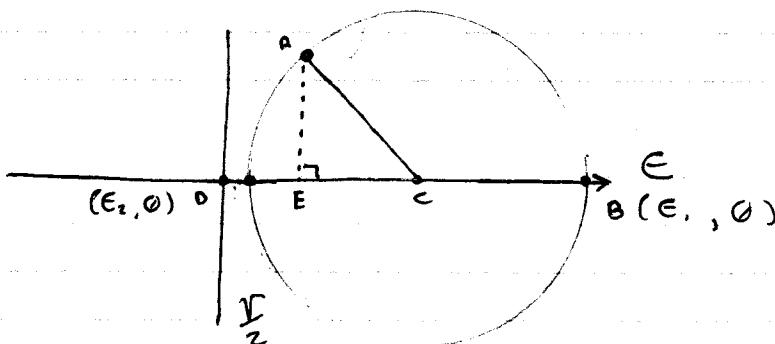
Mohr's Circle :

$$\epsilon_{avg} = \frac{\epsilon_x + \epsilon_y}{2} = \frac{60 + 246}{2}(10^{-6}) \\ = 153(10^{-6})$$

$$\therefore \text{centre } C(\epsilon_{avg}, \theta) = C(153(10^{-6}), \theta)$$

$$\text{Reference Point A } (\epsilon_x, \frac{1}{2}\tau_{xy})$$

$$= (60 \times 10^{-6}, -74.5 \times 10^{-6})$$



Radius

$$R = \sqrt{\left(\frac{\epsilon_x - \epsilon_y}{2}\right)^2} \dots \text{etc. use formula.}$$

$$R = 119.2(10^{-6})$$

$$\therefore \epsilon_1 = \epsilon_{avg} + R = 153(10^{-6}) + 119.20(10^{-6}) \\ = 272.2(10^{-6})$$

$$\epsilon_2 = \epsilon_{avg} - R = 153(10^{-6}) - 119.20(10^{-6}) \\ = 33.8(10^{-6})$$

(2)

$$\triangle ACE: \quad AE = 74.5 (10^{-6})$$

$$CE = 153 (10^{-6}) - 60 (10^{-6})$$

$$= 93 (10^{-6})$$

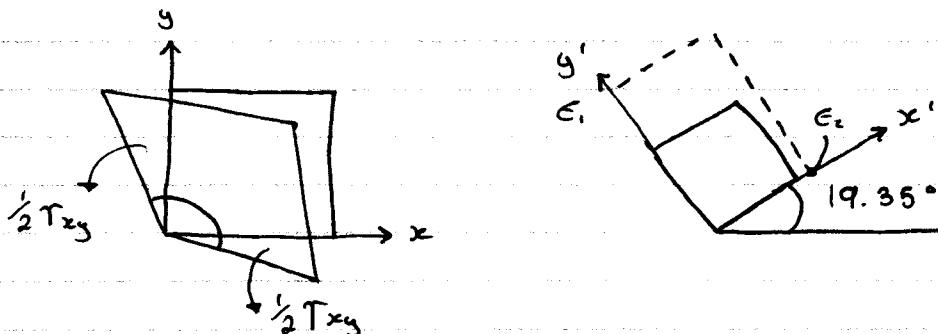
$$\therefore \tan \angle ACE = \frac{AE}{CE} = \frac{74.5 (10^{-6})}{93 (10^{-6})}$$

$$\angle ACE = 38.7^\circ$$

$$\therefore 2\theta_{P2} = \angle ACE = 38.7^\circ$$

$$\theta_{P2} = 19.35^\circ$$

$$\text{and } \theta_{P1} = 90^\circ + 19.35^\circ = 109.35^\circ$$



10.6 Material Property Relationships

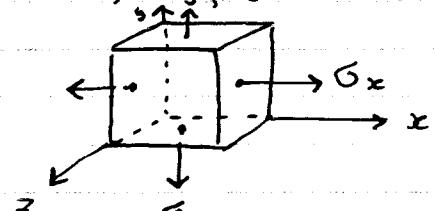
General Hooke's Law

↪ A 3D state of stress

Normal Stress and Normal Strains

$$\sigma_x, \sigma_y, \sigma_z$$

$$\epsilon_x, \epsilon_y, \epsilon_z$$



$$\epsilon_x = \frac{\sigma_x}{E}$$

$$\epsilon_y = -\nu \epsilon_x = -\frac{\nu \sigma_x}{E}$$

$$\epsilon_z = -\nu \epsilon_x = -\frac{\nu \sigma_x}{E}$$

$$\epsilon_x = -\nu \epsilon_y = -\frac{\nu \sigma_y}{E}$$

$$\epsilon_y = \frac{\sigma_x}{E}$$

$$\epsilon_z = -\nu \epsilon_y = -\frac{\nu \sigma_y}{E}$$

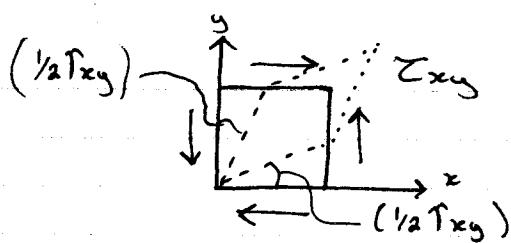
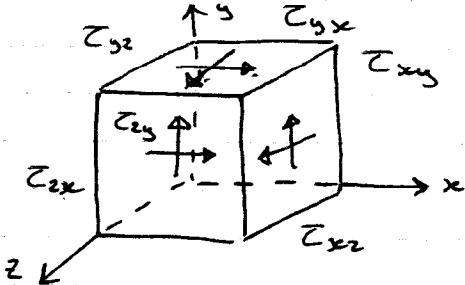
$$\epsilon_x = -\nu \epsilon_z = -\frac{\nu \sigma_z}{E}$$

$$\epsilon_z = \frac{\sigma_x}{E}$$

$$\epsilon_y = -\nu \epsilon_z = -\frac{\nu \sigma_z}{E}$$

$$\left\{ \begin{array}{l} \epsilon_x = \frac{\sigma_x}{E} - \nu \sigma_y - \nu \sigma_z = \frac{1}{E} [\sigma_x - \nu(\sigma_y + \sigma_z)] \\ \epsilon_y = -\nu \sigma_x + \frac{\sigma_y}{E} - \frac{2\sigma_z}{E} = \frac{1}{E} [\sigma_y - \nu(\sigma_z + \sigma_x)] \\ \epsilon_z = -\nu \sigma_x - \frac{\nu \sigma_y}{E} + \frac{\sigma_z}{E} = \frac{1}{E} [\sigma_z - \nu(\sigma_x + \sigma_y)] \end{array} \right.$$

Shear stress and shear strain:



$$\left\{ \begin{array}{l} \tau_{xy} = \frac{\tau_{xy}}{G} \\ \tau_{yz} = \frac{\tau_{yz}}{G} \\ \tau_{zx} = \frac{\tau_{zx}}{G} \end{array} \right.$$

Principal Stress and Principal Strain:

$$\begin{array}{c} xy \leftrightarrow \text{Principal stress directions} \\ \leftrightarrow \tau_{xy} = \tau_{yz} = \tau_{zx} = 0 \end{array}$$

Hooke's Law

$$\begin{array}{c} \leftrightarrow \tau_{xy} = \tau_{yz} = \tau_{zx} = 0 \\ \leftrightarrow \text{Principal stress directions} \end{array}$$

Furthermore,

$$\begin{array}{l} \sigma_1, \sigma_2, \sigma_3 ; \epsilon_1, \epsilon_2, \epsilon_3 \\ \Leftrightarrow \epsilon_1 = \frac{1}{E} [\sigma_1 - \nu(\sigma_2 + \sigma_3)] \end{array}$$

$$\epsilon_2 = \frac{1}{E} [\sigma_2 - \nu(\sigma_3 + \sigma_1)]$$

$$\epsilon_3 = \frac{1}{E} [\sigma_3 - \nu(\sigma_1 + \sigma_2)]$$

(4)

Plane Stress and plane strain

Plane stress: $\sigma_z = \tau_{xz} = \tau_{yz} = 0$

Hooke's Law:

$$\epsilon_x = \frac{1}{E} [\sigma_x - \nu(\sigma_y + \sigma_z)] = \frac{\nu}{E} (\sigma_y + \sigma_z) \neq 0$$

$$\tau_{xz} = 0, \tau_{yz} = 0$$

Not a plane strain.

Plane strain $\epsilon_z = 0 \quad \tau_{xz} = \tau_{yz} = 0$

Hooke's Law: $\tau_{xz} = \tau_{yz} = 0$

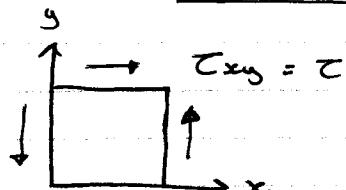
Since $\epsilon_z = \frac{1}{E} [\sigma_z - \nu(\sigma_x + \sigma_y)] = 0$

$$\Rightarrow \sigma_z = \nu(\sigma_x + \sigma_y) \neq 0$$

\rightarrow (Poisson's ratio)

E, U, G
 G (shear modulus)
 $(\text{modulus of elasticity})$

$$\Rightarrow G = \frac{E}{2(1+\nu)}$$

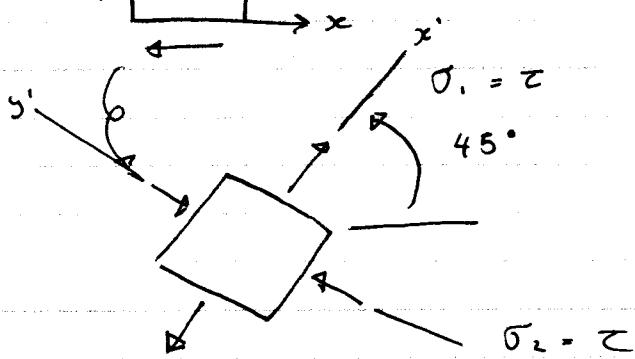


$$\tau_{xy} = \frac{\sigma}{G}$$

$$\epsilon_{x'} = \epsilon_x \cos^2 45^\circ + \epsilon_y \sin^2 45^\circ + \tau_{xy} \sin 45^\circ \cos 45^\circ$$

$$= \frac{1}{2} \tau_{xy}$$

$$\epsilon_{y'} = -\frac{1}{2} \tau_{xy}$$



In x'y': Hooke's Law

$$\epsilon_{x'} = \frac{1}{E} (\sigma_{x'} - \nu \sigma_{y'})$$

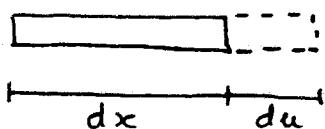
$$\text{Since } \sigma_x' = \epsilon, \quad \sigma_y' = -\epsilon$$

$$\Rightarrow \frac{1}{2} \tau_{xy} = \frac{1}{E} (\epsilon + \nu \epsilon) = \frac{1+\nu}{E} \epsilon$$

$$\Rightarrow \frac{1}{2} \frac{\epsilon'}{G} = \frac{1+\nu}{E} \cdot \frac{\epsilon}{E}$$

$$\boxed{\Rightarrow G = \frac{E}{2(1+\nu)}}$$

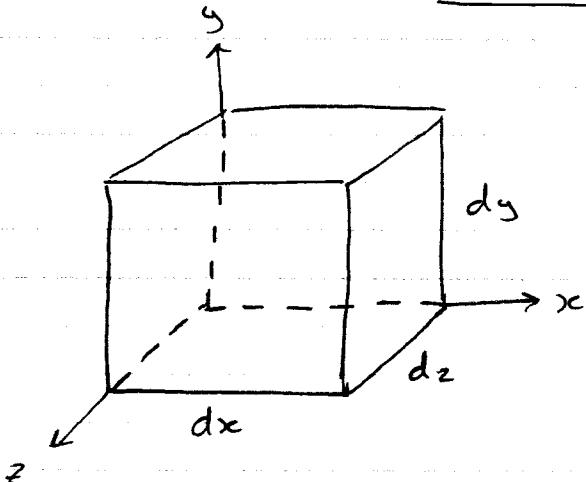
Dilation and Bulk Modules



$$\epsilon_x : \epsilon_x = \frac{du}{dx}$$

$$du = \epsilon_x dx$$

$$\boxed{dx' = du + dx = (1 + \epsilon_x) dx}$$



$$\epsilon_x, \epsilon_y, \epsilon_z$$

$$\begin{aligned} dx &\rightarrow dx' = (1 + \epsilon_x) dx \\ dy &\rightarrow dy' = (1 + \epsilon_y) dy \\ dz &\rightarrow dz' = (1 + \epsilon_z) dz \end{aligned}$$

$$\begin{aligned} \text{Volume old } dV &= dx dy dz \\ \text{new } dV' &= dx' dy' dz' \end{aligned}$$

Volume change

$$\begin{aligned} \delta V &= dV' - dV \\ &= (1 + \epsilon_x)(1 + \epsilon_y)(1 + \epsilon_z) dx dy dz - dV \\ &= (1 + \epsilon_x + \epsilon_y + \epsilon_z + \epsilon_x \epsilon_y + \epsilon_y \epsilon_z + \epsilon_z \epsilon_x \\ &\quad + \epsilon_x \epsilon_y \epsilon_z) dV - dV \\ &= (\epsilon_x + \epsilon_y + \epsilon_z) dV \end{aligned}$$

Volumetric Strain \longleftrightarrow dilation

$$\epsilon = \frac{\delta V}{dV} = \epsilon_x + \epsilon_y + \epsilon_z$$

(6)

Hooke's Law

$$\epsilon_x = \frac{1}{E} (\sigma_x - \nu(\sigma_y + \sigma_z))$$

$$\epsilon_y = \frac{1}{E} (\sigma_y - \nu(\sigma_z + \sigma_x))$$

$$\epsilon_z = \frac{1}{E} (\sigma_z - \nu(\sigma_x + \sigma_y))$$

$$\epsilon_x + \epsilon_y + \epsilon_z = \frac{1-2\nu}{E} (\sigma_x + \sigma_y + \sigma_z)$$

Bulk modulus:

$$\text{IF } \sigma_x = \sigma_y = \sigma_z = -P$$

$$E = -\frac{3(1-2\nu)}{E} P$$

$$\frac{P}{E} = -\frac{1}{3(1-2\nu)}$$

Define

$$K = \frac{E}{3(1-2\nu)}$$

bulk modulus

$$\Rightarrow P = -K_e$$

No volume change

$$1-2\nu = 0$$

$$\nu = 1/2$$