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- 5 problems
- No m/c (or maybe just a few)
- Tutorials → Assignments
- ↳ review Practice problems

For final

$$1 \text{ Pa} = \frac{1 \text{ N}}{\text{m}^2} \Rightarrow \frac{\text{kg}}{\text{m} \cdot \text{s}^2}$$

$$\text{N} = 1 \frac{\text{kg} \cdot \text{m}}{\text{s}^2}$$

Example:

$$\Delta P = f\{R, \bar{v}\}$$

$$\Delta P \quad R \quad \bar{v}$$

$$\{ml^{-1}t^{-2}\} \quad \{L\} \quad \{mt^{-2}\}$$

$$n = n_{-s} = 0$$

$$n = 3$$

$$\cancel{2=3}$$

$$3=2$$

$$\text{then } n = 3-2 = 1$$

$$\Pi_1 = \frac{\Delta P \cdot R}{\bar{v}}$$

$$\left( \frac{m}{L t^2} \right) \left( L \right) \left( \frac{m}{t^2} \right)^{-1} \cancel{2}$$

$$\left( \frac{m}{L t^2} \right) \left( L \right) \left( t^2/m \right) = 1$$

$$\text{thus } \Pi_1 = \frac{\Delta P \cdot R}{\bar{v}}$$

When there's just 1 dimensionless number, that number is equal to a constant.

Example:

$$F_L = f(V, L_c, \rho, \mu, C, \alpha) \quad n = 7$$

$$F_L \quad V \quad L_c \quad \rho \quad \mu \quad C \quad \alpha$$

$$\{kg \cdot m/s^2\} \quad \{m/s\} \quad \{m\} \quad \{kg/m^3\} \quad \{m/s\} \quad \{m/s\} \quad \{1\}$$

$$\text{then } \cancel{3} = 3$$

$$7-3 = 4, \text{ then rep. var.} = V, L_c, \rho$$

$$\text{then } \Pi_1 = F_L \cdot V \cdot L_c \cdot \rho$$

$$\left( \frac{(kg \cdot m)}{s^2} \right) \left( \frac{m}{s} \right) \left( m \right) \left( \frac{kg}{m^3} \right)^{-1}$$

$$\left( \frac{kg \cdot m}{s^2} \right) \left( \frac{s^2}{m^2} \right) \left( m^2 \right) \left( \frac{m^3}{kg} \right) \cancel{2}$$

$$\left( \frac{kg \cdot m}{s^2} \right) \left( \frac{s^2}{m^2} \right) \left( \frac{1}{m^2} \right) \left( \frac{m^3}{kg} \right) = 1$$

$$\text{then } \Pi_1 = \frac{F_L}{V^2 \cdot L_c^2 \cdot \rho}$$

$$\text{Then } \Pi_{1, \text{modified}} = \frac{F_L}{(\gamma_2) V^2 A P} = C_L \rightarrow \text{since } L \times L = A \\ (\gamma_2) \text{ is constant}$$

$$\begin{aligned} \Pi_2 &= \mu \cdot V \cdot L_c \cdot \rho \\ &= \left( \frac{\text{kg}}{\text{m} \cdot \text{s}} \right) \left( \frac{\text{m}}{\text{s}} \right) \left( \text{m} \right) \left( \frac{\text{kg}}{\text{m}^3} \right)^{-1} \\ &= \left( \frac{\text{kg}}{\text{m} \cdot \text{s}} \right) \left( \frac{\text{kg}}{\text{m}^2} \right) \left( \frac{1}{\text{m}} \right) \left( \frac{\text{m}^3}{\text{kg}} \right) = 1 \\ \text{then } \Pi_2 &= \frac{\mu}{V \cdot L_c \cdot \rho} \end{aligned}$$

$\Pi_2, \text{modified} = Re \rightsquigarrow$  Reynolds number, inverse

$$\begin{aligned} \Pi_3 &= C \cdot V \cdot L_c \cdot \rho \\ &= \left( \frac{\text{m}}{\text{s}} \right) \left( \frac{\text{m}}{\text{s}} \right) \left( \text{m} \right) \left( \frac{\text{kg}}{\text{m} \cdot \text{s}} \right)^0 \\ &= \left( \frac{\text{m}}{\text{s}} \right) \left( \frac{\text{s}}{\text{m}} \right) (1)(1) = 1 \\ \Pi_3 &= \frac{C}{V} \end{aligned}$$

then  $\Pi_3, \text{modified} = \frac{V}{C} \rightsquigarrow$  Mach number, inverse

$$\begin{aligned} \Pi_4 &= \alpha \cdot V \cdot L_c \cdot \rho \\ &= (1) \left( \frac{\text{m}}{\text{s}} \right) \left( \text{m} \right) \left( \frac{\text{kg}}{\text{m}^3} \right)^0 \end{aligned}$$

$$\Pi_4 = \alpha$$

$\text{thus, } C_L = f(Re, Ma, \alpha)$

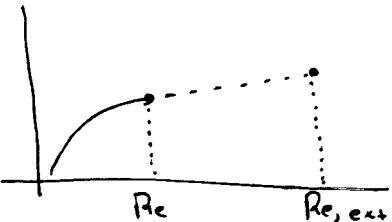
Complete set of experiments (called Full Factorial test matr:  $X$ )

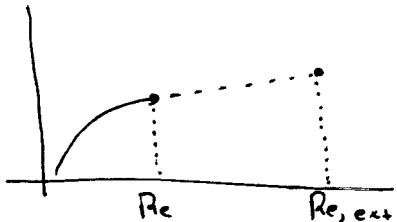
If 5 dependent variables initially, complete set would be  $5^4 = 625$

Using non-dimensional analysis,  $K = 5 - 3 = 2$

then dependent variable = 1, thus new complete set  $5^1 = 5$

- allows fewer experiments to return the same resolution.
- Not always possible to match all <sup>the nodes</sup> TC to TT's of Prototype : called incomplete similarity.

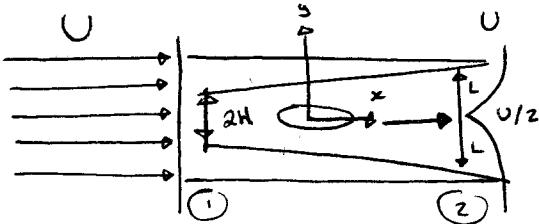
 extrapolating results : result needs more testing



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Example :



$$\textcircled{1} \quad y = 0 \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$u = U/2 \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$\textcircled{2} \quad y = L \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$u = U \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$\frac{\partial}{\partial t} \int_{\text{vol}} \rho dV + \int_{\text{cs}} \rho (\vec{v} \cdot \vec{n}) dA = 0$$

$$\rightarrow \int_{\text{sec 2}} \rho u dA - \int_{\text{sec 1}} \rho u dA = 0$$

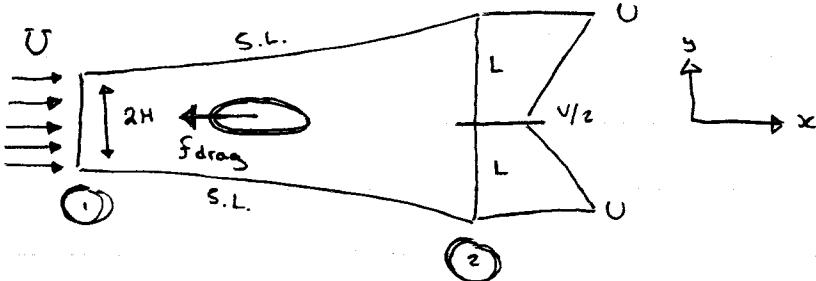
$$2 \int_0^L \rho \frac{U}{2} (1 + \frac{y}{L}) b dy - \int_0^H 2 \rho U b dy = 0$$

$$2 \rho \frac{U}{2} b \int_0^L (1 + \frac{y}{L}) dy - 2 \rho U b H$$

$$2 \rho \frac{U}{2} b \left[ y + \frac{y^2}{2L} \Big|_{y=0}^{y=L} \right] - 2 \rho U b H = 0$$

$$2 \rho \frac{U}{2} b \left[ L + \frac{L^2}{2L} \right] - 2 \rho U b H = 0$$

$$H = 3L/4$$



$$-F_{\text{drag}} = \frac{\partial}{\partial t} \int_{\text{vol}} \rho v dV + \int_{\text{cs}} \rho V_p (\vec{v} \cdot \vec{n}) dA$$

$$-F_{\text{drag}} = \int_{\text{sec 2}} \rho u v dA - \int_{\text{sec 1}} \rho u v dA$$

$$-F_{\text{drag}} = 2 \int_0^L \frac{U}{2} (1 + \frac{y}{L}) \rho \frac{U}{2} (1 + \frac{y}{L}) b dy - 2 \int_0^H U \rho U b dy$$

$$-F_{\text{drag}} = 2 \frac{U^2}{4} \rho b \int_0^L (1 + \frac{y}{L})^2 dy - 2 U^2 \rho b H$$

$$\int_0^L (1 + \frac{2y}{L} + \frac{y^2}{L^2}) dy = y + \frac{2y^2}{2L} + \frac{y^3}{3L^2} \Big|_0^L$$

$$L + \frac{2L^2}{2L} \dots$$

$\frac{7}{3} L$  } Tarokh got confused  
and stopped.

$$-F_{\text{drag}} = 2 \frac{U^2}{4} \rho b (\frac{7}{3}) L - 2 U^2 \rho b (\frac{3}{4}) L$$

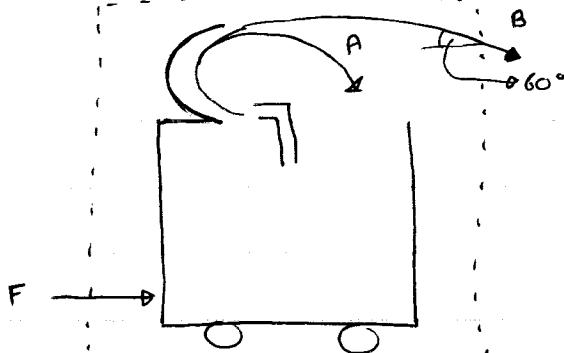
$$F = (\frac{1}{3}) \rho V^2 L b \quad \rightarrow \quad C_D = \frac{F_{\text{drag}}}{(\frac{1}{2}) \rho V^2 L b} \approx C_D = \frac{(\frac{1}{3})}{(\frac{1}{12})} = \frac{2}{3}$$

b)  $F_{\text{drag}} = \frac{1}{3} \rho v^2 L b$

$$F_{\text{drag}} = \left(\frac{1}{3}\right)(998)(4)^2 (0.8)(1) = 4260 \text{ N}$$

$C_D$  is still  $2/3$  (doesn't change)

Example:



For A)  $\sum F_x = \frac{\partial}{\partial t} \int_{\text{cv}} \rho v dV + \underbrace{\int_{\text{cs}} \rho v (\bar{v} \cdot \bar{n}) dA}_{\emptyset}$

$$\sum F_x = \emptyset = f$$

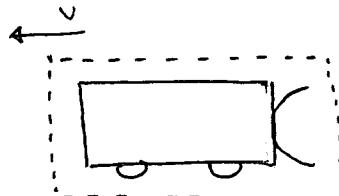
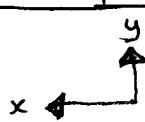
For B)  $\sum F_x = \frac{\partial}{\partial t} \cancel{\int_{\text{cv}} \rho v dV} + \int_{\text{cs}} \rho v (\bar{v} \cdot \bar{n}) dA$

$$F = \emptyset + (m V_{x,\text{out}} - \emptyset)$$

$$F = (1.94 \text{ slug}/\text{ft}^3) \left( \frac{200}{448} \text{ ft}^3/\text{s} \right) (45 \cos 60^\circ)$$

$F = 19.5 \text{ lb}_f$

**Example**



$$\sum F_x = \frac{\partial}{\partial t} \int_{cv} \rho v dV + \int_{cs} \rho V_x (\bar{v} \cdot \bar{n}) dA$$

$$\textcircled{1} = \frac{\partial}{\partial t} \int_{cv} v dm + \int_{cs} \rho V_x (\bar{v} \cdot \bar{n}) dA$$

$$\textcircled{2} = \frac{\partial}{\partial t} v \int_{cv} dm + m_{out} u_{out} - m_{in} u_{in}$$

$$\textcircled{3} = \frac{\partial v}{\partial t} m_{car} - 2 \dot{m} (V_s - v) \quad (V_s = \text{velocity of jet}) \\ = \frac{\partial v}{\partial t} m_{car} - 2 \rho A_s (V_s - v)^2$$

$$\frac{dv}{dt} m_{car} = 2 \rho A_s (V_s - v)^2$$

$$\frac{dv}{dt} = \frac{2 \rho A_s (V_s - v)^2}{m_{car}} = K (V_s - v)^2$$

$$K = \frac{2 \rho A_s}{m_{car}}$$

$$\frac{dv}{dt} = K (V_s - v)^2$$

$$\int \frac{dv}{(V_s - v)^2} = \int K dt \rightarrow \frac{1}{V_s - v} + C = Kt$$

$$t=0 \Rightarrow \frac{1}{V_s - 0} + C = 0 \Rightarrow C = -\frac{1}{V_s}$$

$$\frac{1}{V_s - v} - \frac{1}{V_s} = Kt \quad \Rightarrow$$

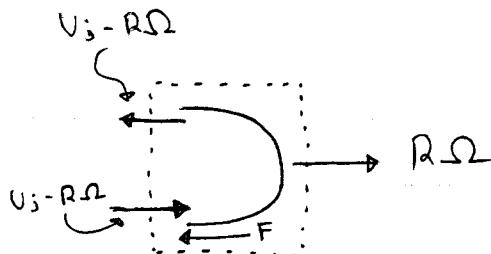
$$V = \frac{V_s^2 K t}{1 + V_s K t}$$

$$K = \frac{2 \rho A_s}{m_{car}} = \frac{2(998)(\pi/4)(0.01)^2}{(12/9.81)} \Rightarrow K = 0.0905 \text{ m}^{-1}$$

$$V = \frac{(509t)}{1 + 6.785t} \quad \Rightarrow \quad \left. \begin{array}{l} x = 1 \\ t = ? \end{array} \right\} 0.072 \text{ s} \Rightarrow V = 24.6 \text{ m/s}$$

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**Example**

$$\sum F_x = \dot{m} u_{out} - \dot{m} u_{in}$$

$$= \dot{m}(-(V_3 - R\Omega)) - \dot{m}(V_3 - R\Omega)$$

$$-F = -2\dot{m}(V_3 - R\Omega)$$

$$F = 2\dot{m}(V_3 - R\Omega)$$

$$IP = T\Omega$$

$$IP = FR\Omega$$

$$IP = 2\dot{m}(V_3 - R\Omega)R\Omega$$

$$\dot{m} = \rho A_3(V_3 - R\Omega)$$

$$IP = 2\rho A_3 R\Omega (V_3 - R\Omega)^2$$

$$\frac{dP}{d\Omega} = 0 = \frac{d}{d\Omega}(2\rho A_3 R\Omega (V_3 - R\Omega)^2) = 0$$

$$2\rho A_3 R \frac{d}{d\Omega}(\Omega(V_3 - R\Omega)^2) = 0$$

$$(V_3 - R\Omega)^2 + 2\Omega(-R)(V_3 - R\Omega) = 0$$

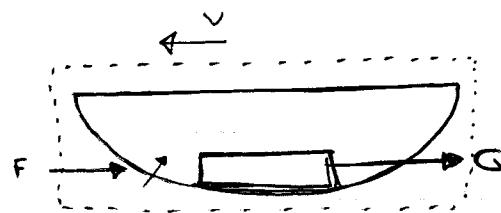
$$(V_3 - R\Omega)(V_3 - R\Omega - 2R\Omega) = 0$$

$$(V_3 - R\Omega)(V_3 - 3R\Omega) = 0$$

$$\boxed{R\Omega = V_3/3}$$

$$IP_{max} = 2\rho A_3(V_3/3)(V_3 - V_3/3)^2 = \underline{(8/27)\rho A_3 V_3^3}$$

**Example:**



$$\sum F_x = \dot{m} u_{out} - \dot{m} u_{in}$$

$$KV^2 = \dot{m}_{pump} (V_s - V_{inlet} + V) = \rho Q (V_s - V_{inlet} + V)$$

$$V_{inlet} \ll V \text{ & } V_s$$

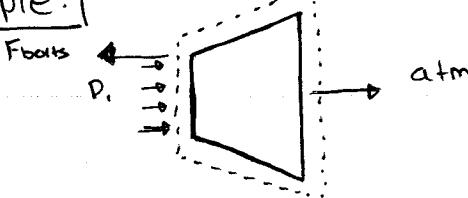
$$KV^2 = \rho Q (V_s + V)$$

$$V^2 = \frac{\rho Q}{\mu} (V_s + V) \Rightarrow V^2 - \frac{\rho Q}{\mu} V - \frac{\rho Q}{\mu} \cdot V_s = 0$$

$$\frac{\rho Q}{2\mu} = \alpha \Rightarrow V = \alpha + (\alpha^2 + 2\alpha V_s)^{1/2}$$

$$\text{assume } V \ll V_s \Rightarrow KV^2 = \rho Q V_s$$

**Example:**



$$\frac{P_1}{\rho} + \frac{V_1^2}{2} + gZ_1 = \frac{P_2}{\rho} + \frac{V_2^2}{2} + gZ_2$$

$$V_1 = \omega / (\pi/4)(0.1)^2 = 12.73 \text{ m/s}$$

$$V_2 = \omega / (\pi/4)(0.2)^2 = 3.18 \text{ m/s}$$

$$\begin{aligned} \text{From } (1) \Rightarrow P_1 &= (1/2)\rho(V_2^2 - V_1^2) \\ &= (1/2)(1000)(3.18^2 - 12.73^2) \\ \Rightarrow P_{1, \text{gauge}} &= 75970 \text{ Pa} \end{aligned}$$

$$\sum F_x = \dot{m} u_{out} - \dot{m} u_{in}$$

$$P_1 A_1 - F_{bolts} = \dot{m}(V_2 - V_1)$$

$$F_{bolts} = (75970)(\pi/4)(0.1)^2 - (1000)(0.1)(3.18 - 12.73)$$

$$F_{bolts} = 1552 \text{ N}$$